

UNCLASSIFIED COPY
NO CALL
10/15

OPTIMUM RANGES FOR X-RAY THICKNESS MEASUREMENTS

Richard W. Ryon

October 15, 1985

Lawrence
Livermore
National
Laboratory

This is an informal report intended primarily for internal or limited external distribution. The opinions and conclusions stated are those of the author and may or may not be those of the Laboratory.

Work performed under the auspices of the U.S. Department of Energy by the Lawrence Livermore National Laboratory under Contract W-7405-Eng-48.

DISCLAIMER

This document was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor the University of California nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial products, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or the University of California, and shall not be used for advertising or product endorsement purposes.

Printed in the United States of America
Available from
National Technical Information Service
U.S. Department of Commerce
5285 Port Royal Road
Springfield, VA 22161
Price: Printed Copy \$ Microfiche \$4.50

Page Range	Domestic Price	Page Range	Domestic Price
001-025	\$ 7.00	326-350	\$ 26.50
026-050	8.50	351-375	28.00
051-075	10.00	376-400	29.50
076-100	11.50	401-426	31.00
101-125	13.00	427-450	32.50
126-150	14.50	451-475	34.00
151-175	16.00	476-500	35.50
176-200	17.50	501-525	37.00
201-225	19.00	526-550	38.50
226-250	20.50	551-575	40.00
251-275	22.00	576-600	41.50
276-300	23.50	601-up ¹	
301-325	25.00		

¹Add 1.50 for each additional 25 page increment, or portion thereof from 601 pages up.

OPTIMUM RANGES FOR X-RAY THICKNESS MEASUREMENTS

Richard W. Ryon
Lawrence Livermore National Laboratory
Livermore, California 94550

As illustrated in Figure 1, film thicknesses can be measured by two x-ray methods:

- 1) X-ray absorption (gauging or radiography). The incident beam passes through the material, and the attenuation of the beam by the material is measured.
 - 2) X-ray fluorescence. If the material consists of elements which fluoresce in the accessible region of the x-ray spectrum, the intensity of that fluorescence is related to thickness. There are three possibilities.
 - a) The fluorescence of a material behind the specimen can be measured. This is analogous to (1) above.
 - b) Source and detector are both on the same side of the specimen.
 - c) Source and detector are on opposite sides of the specimen.
-

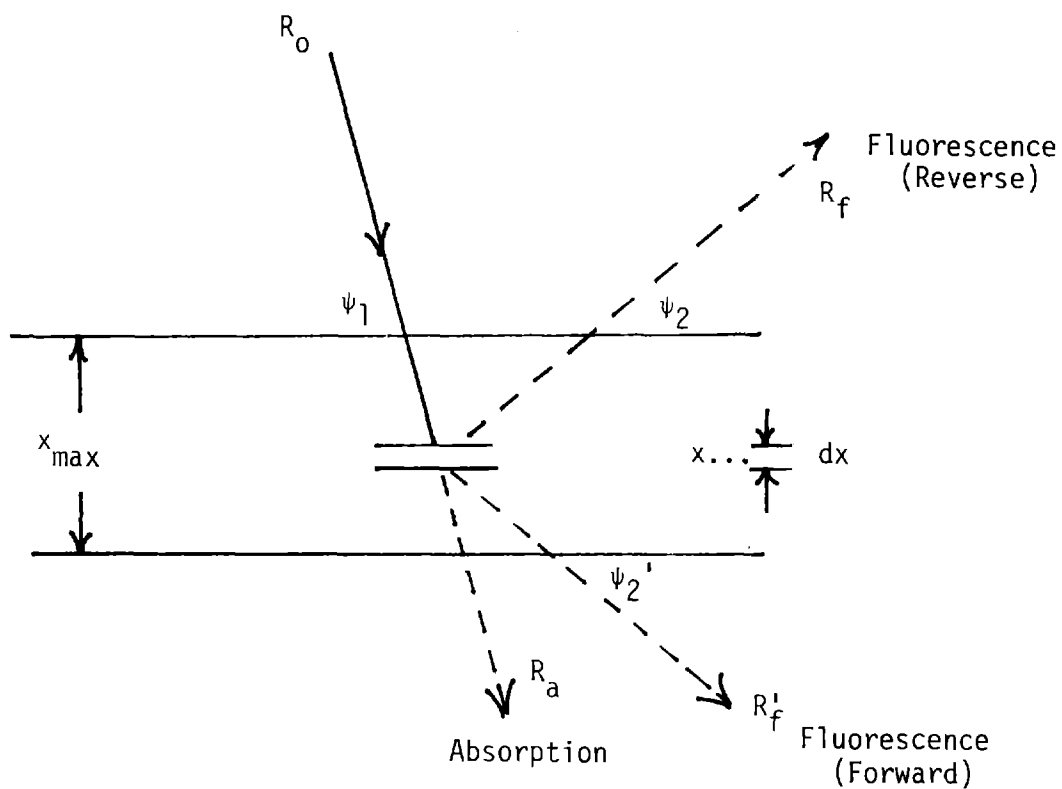


Figure 1. Thickness measurement by absorption (R_a), by fluorescence in the back direction (R_f), and by fluorescence in the forward direction (R_f').

A rule-of-thumb used in absorption measurements is that the best precision is obtained when the incident beam is attenuated by e^{-2} (that is, $\mu\rho x = 2$).

Questions which arise are:

- 1) What are the analogous rule-of-thumb for fluorescence measurements (forward and reverse directions)?
- 2) What happens to precision at non-optimum thickness? Over what ranges are the methods best applied?

The answers are summarized in the table below. The remainder of this note provides the methodology and equations used to obtain the results.

	Optimum $\mu\rho x$	Minimum error when $N_{\max}=10^5$	Range of $\mu\rho x$ to double error	Range for Gold*
Absorption	2.0	.43%	.46-5.4	7.9-93 mg/cm^2
Fluorescence-Rev.	.64	.64%	.067-2.3	0.37-13 mg/cm^2
Fluorescence-For.	.57	.67%	.067-1.5	0.37-8.3 mg/cm^2

*Assuming silver incident radiation

$$\mu_{\text{AgK}\alpha, \text{Au}} = 58$$

$$\mu_{\text{AuL}\alpha, \text{Au}} = 123$$

90° geometry

Sensitivity to Change in Areal Density

The equations for absorption and fluorescence are very similar. In fact, the curves in figure 2 are mirror images of each other.

$$\text{Absorption: } R/R_0 = e^{-\mu\rho x}$$

$$\text{Fluorescence: } R/R_0 = 1 - e^{-\mu\rho x}$$

where R = counting rate from the specimen

R_0 = maximum counting rate. For absorption, this is the incident beam intensity (i.e., no specimen).

For fluorescence, the maximum rate is obtained at "infinite" thickness.

We want a large change in relative counting rate per unit change in areal density so that we can distinguish between small increments of areal density.

The sensitivity is found by differentiations:

$$\text{Absorption: } \frac{d(R/R_0)}{d(\rho x)} = -\mu e^{-\mu\rho x}$$

$$\text{Fluorescence: } \frac{d(R/R_0)}{d(\rho x)} = \mu e^{-\mu\rho x}$$

We see from these equations (and from Figure 2), that the greatest sensitivity is when the areal density approaches zero (that is,

$d(R/R_0)/d(\rho x)$ approaches $|\mu|$. Conversely, the sensitivity approaches zero as the thickness increases toward "infinity."

Clearly, the area to be avoided is that of thick specimens where the sensitivity approaches zero. One might conclude that the converse is true, that the best measurements are made with thin specimens, where the sensitivity in the measured parameter (R/R_0) is greatest. Further reflection indicates this idea is not valid.

When the specimen is very thin, there is very little to measure. In the fluorescence case, the counting rate is small and the counting statistics are poor. With absorption, the counting rate is at its highest, but the error in the number of counts represents a large relative error in the areal density.

We therefore conclude that there is an optimum range of thicknesses for measurement, somewhere between the extremes of very thin and very thick specimens. What follows is the calculation of the optimum ranges.

Equations for Fluorescence in the Forward and Reverse Directions:

(Refer to Figure 1)

1) The primary beam is attenuated

passing through the material

to the infinitesimal dx : $Attn_1 = (e^{-\mu_1 \rho x})$

2) At dx , fluorescence occurs: $dI = I_0' K' C \rho dx$

3) The fluorescent beam is
attenuated as it passes
out of the material:

$$\text{Attn}_2(\text{rev}) = e^{-\mu_2 \rho x}$$

$$\text{Attn}_2(\text{for}) = e^{-\mu_2 \rho (x_{\text{max}} - x)}$$

where μ_1 = mass abs. coef. for the primary radiation, corrected for path length ($\csc \psi_1$)
 μ_2 = mass abs. coef. for the fluorescent radiation, corrected for path length ($\csc \psi_2$)
 K' = sensitivity factor, usually empirically determined from a standard material
 C = weight fraction of the fluorescent element
 ρ = density
 x = thickness

The fluorescent intensity is found by combining the factors and integrating over the thickness of the material:

$$dI = I_0' \text{Attn}_1 \times \text{Attn}_2 \times K' C \rho dx$$

$$\text{Reverse: } \int_0^R dI = I_0' K' C \rho \int_0^{x_{\text{max}}} e^{-(\mu_1 + \mu_2) \rho x} dx$$

$$R = \frac{KC}{\mu_1 + \mu_2} \left(1 - e^{-(\mu_1 + \mu_2)\rho x_{\max}} \right)$$

$$R = R_0 \left(1 - e^{-\mu \rho x_{\max}} \right)$$

where $\mu = \mu_1 + \mu_2$

$$R_0 = \text{intensity at "infinite" thickness} = \frac{KC}{\mu}$$

Forward: $dI = I_0 K' C \rho e^{-\mu_1 \rho x} e^{-\mu_2 (x_{\max} - x) \rho} dx$

$$\int_0^R dI = I_0 K' C \rho e^{-\mu_2 \rho x_{\max}} \int_0^{x_{\max}} e^{-(\mu_1 - \mu_2) \rho x} dx$$

$$R = \frac{K' C I_0}{(\mu_1 - \mu_2)} e^{-\mu_2 \rho x_{\max}} \left(1 - e^{-(\mu_1 - \mu_2) \rho x_{\max}} \right)$$

$$R = \frac{KC}{(\mu_1 - \mu_2)} \left(e^{-\mu_2 \rho x_{\max}} - e^{-\mu_1 \rho x_{\max}} \right)$$

In limiting cases, the two equations become identical:

$$1) \quad \mu_1 \rightarrow 0 \quad R_{\text{for}} \rightarrow R_{\text{rev}} = \frac{KC}{\mu_2} \left(1 - e^{-\mu_2 \rho x} \right)$$

$$2) \quad \rho x \rightarrow 0 \quad R_{\text{for}} \rightarrow R_{\text{rev}} = KC \rho x$$

The functional relationships between relative intensities and areal densities are plotted in Figure 2.

Find the minimum in measurement error as a function of areal density:

We seek the fractional error in the areal density measurement as a function of the number of counts in some given time. Once we know the functional relationship, we can find its minimum, and thus the optimum areal density for measurement.

1) Absorption: Basic eqn: $R/R_0 = e^{-\mu\rho x}$

The counting rate is: $R = N/t$

So that: $\frac{N}{R_0 t} = e^{-\mu\rho x}$

$$\begin{aligned}\text{Solving for areal density: } (\rho x) &= -\frac{1}{\mu} \cdot \ln\left(\frac{N}{R_0 t}\right) \\ &= -\frac{1}{\mu} \left\{ \ln(N) - \ln(R_0 t) \right\}\end{aligned}$$

Find the sensitivity of areal density to changes in the numbers of counts:

$$\frac{d(\rho x)}{dN} = -\frac{1}{\mu} \cdot \frac{1}{N}$$

$$d(\rho x) = -\frac{1}{\mu} \cdot \frac{1}{N} \cdot dN$$

INTENSITY - THICKNESS PROFILES

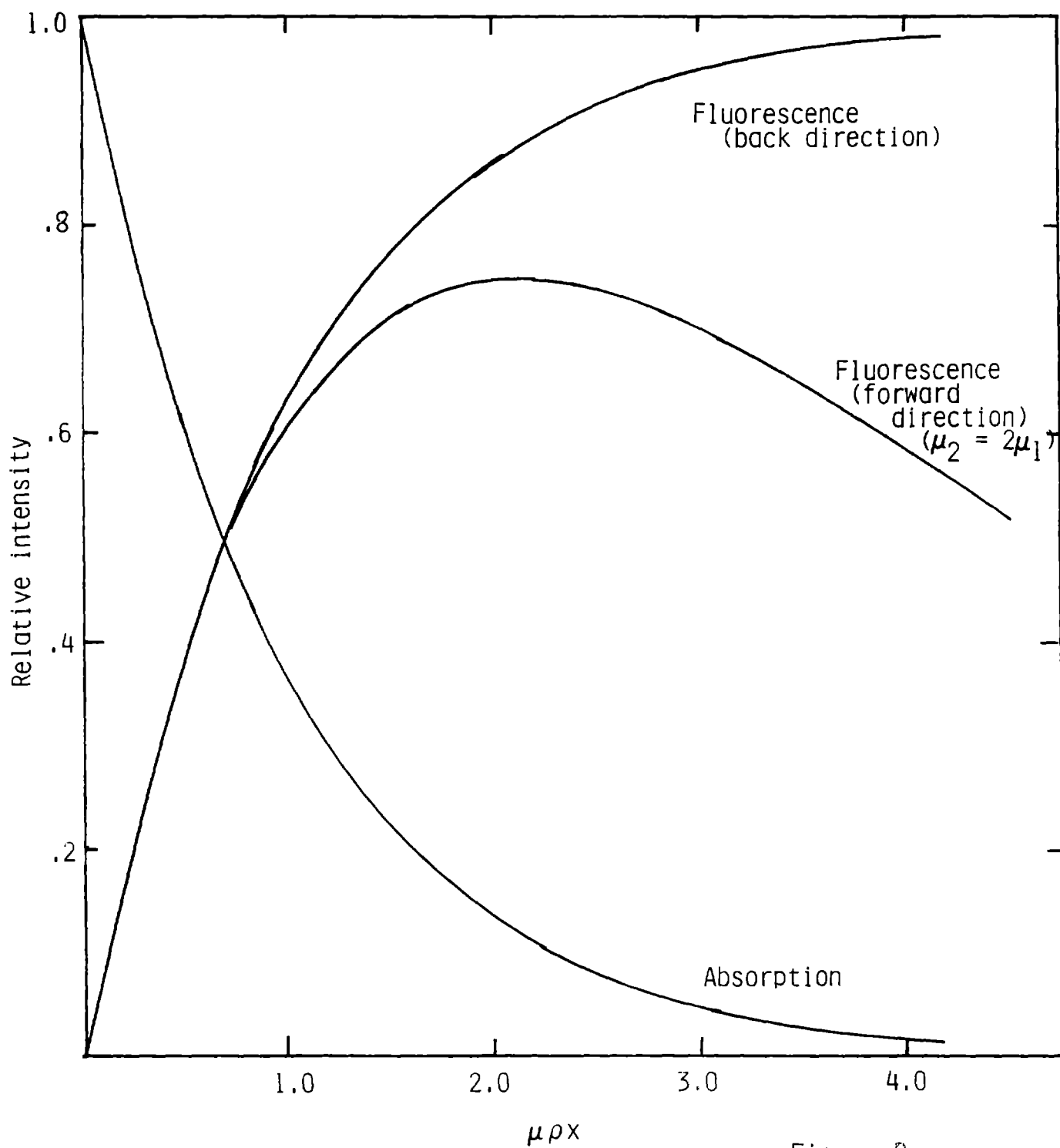


Figure 2

As a fraction:

$$\frac{d(\rho x)}{(\rho x)} = - \frac{1}{\mu \rho x} \cdot \frac{1}{N} \cdot dN$$

The error in the number of counts is $N^{1/2} \equiv \Delta N$:

$$\begin{aligned} \frac{\Delta(\rho x)}{(\rho x)} &= - \frac{1}{\mu \rho x} \cdot \frac{1}{N^{1/2}} \\ &= \frac{1}{\ln(R/R_0)} \cdot \frac{1}{N^{1/2}} \end{aligned}$$

We next seek the minimum in fractional error:

$$\begin{aligned} \frac{d}{dN} \left(\frac{\Delta(\rho x)}{\rho x} \right) &\equiv 0 = \frac{d}{dN} \left\{ \frac{1}{N^{1/2}} \cdot \frac{1}{\ln(R/R_0)} \right\} \\ &= \frac{d}{dN} \left\{ \frac{1}{N^{1/2}} \cdot \frac{1}{\ln(N) - \ln(R_0 t)} \right\} \\ 0 &= - \frac{1}{2} \cdot \frac{1}{\ln(R/R_0) N^{3/2}} - \frac{1}{(\ln(R/R_0))^2 N^{3/2}} \\ R/R_0 &= e^{-2} \end{aligned}$$

Therefore, the optimum measurement of areal density as measured by absorption is made when $\mu \rho x = 2$.

If we define the optimum range of thickness as that which limits the error to 2 times the minimum:

$$\sigma_{\min} = -\frac{1}{2} \cdot \frac{1}{N^{1/2}}$$

$$2\sigma_{\min} = -\frac{1}{N^{1/2}} = -\frac{1}{\mu\rho x'} \cdot \frac{1}{(N')^{1/2}}$$

$$N^{1/2} = (N')^{1/2} \mu\rho x'$$

$$(R_0 t e^{-\mu\rho x})^{1/2} = (R_0 t e^{-\mu\rho x'})^{1/2} \cdot \mu\rho x'$$

$$.3679 = (e^{-\mu\rho x'})^{1/2} \cdot \mu\rho x'$$

By iterative guesses,

$$\mu\rho x' = .4633 \text{ and } 5.357$$

$$R'/R_0 = .629 \text{ and } .00472$$

2) Fluorescence, reverse direction

$$\text{Basic eqn: } R/R_0 = 1 - e^{-\mu\rho x}$$

$$\text{The count rate is: } R = N/t$$

$$\text{so that: } \frac{N}{R_0 t} = 1 - e^{-\mu\rho x}$$

Solving for areal density:

$$\rho x = -\frac{1}{\mu} \ln\left(1 - \frac{N}{R_0 t}\right)$$

Find the sensitivity of the areal density to changes in the number of counts:

$$\begin{aligned}\frac{d(\rho x)}{dN} &= \frac{1}{\mu} \cdot \frac{1}{1 - N/R_0 t} \cdot \frac{1}{R_0 t} \\ &= \frac{1}{\mu} \cdot \frac{1}{1 - R/R_0} \cdot \frac{R}{R_0 N}\end{aligned}$$

$$d(\rho x) = \frac{1}{\mu} \cdot \frac{1}{1 - R/R_0} \cdot \frac{R/R_0}{N} \cdot dN$$

As a fraction: $\frac{d(\rho x)}{\rho x} = \frac{1}{\mu \rho x} \cdot \frac{1}{1 - R/R_0} \cdot \frac{R/R_0}{N} \cdot dN$

The error in the number of counts is $N^{1/2} = \Delta N$:

$$\begin{aligned}\frac{\Delta(\rho x)}{\rho x} &= \frac{1}{N^{1/2}} \cdot \frac{1}{\mu \rho x} \cdot \frac{R/R_0}{(1 - R/R_0)} \\ &= \frac{-1}{N^{1/2}} \cdot \frac{1}{\ln(1 - R/R_0)} \cdot \frac{R/R_0}{(1 - R/R_0)}\end{aligned}$$

We next seek the minimum in the fractional error:

$$\frac{d}{dN} \left(\frac{\Delta(\rho x)}{\rho x} \right) \equiv 0 = \frac{d}{dN} \left\{ \frac{N^{1/2} e^{-N/R_0 t}}{N^{1/2} \cdot \ln(1 - N/R_0 t) (1 - N/R_0 t)} \right\}$$

Make the substitutions:

numerator = u

denominator = v

$$\text{Recall that } d \frac{u}{v} = \frac{v du - u dv}{v^2}$$

The differential will be zero when $v du - u dv = 0$

$$v du = u dv$$

$$N^{1/2} \cdot \ln(1 - R/R_0) (1 - R/R_0) \cdot (-1/R_0 t) =$$

$$\begin{aligned} & (-R/R_0) \left\{ \frac{1}{2} \cdot N^{-1/2} \cdot \ln(1 - R/R_0) (1 - R/R_0) - N^{1/2} \ln(1 - R/R_0) (R/R_0 t) \right. \\ & \left. - \frac{N^{1/2} (1 - R/R_0) (1/R_0 t)}{1 - R/R_0} \right\} \end{aligned}$$

$$1 = \left\{ \frac{R_0 t}{2N} - \frac{1}{(1 - R/R_0)} - \frac{1}{\ln(1 - R/R_0) (1 - R/R_0)} \right\} R/R_0$$

$$1 = \left\{ \frac{1}{2(R/R_0)} - \frac{1}{(1 - R/R_0)} - \frac{1}{\ln(1 - R/R_0) (1 - R/R_0)} \right\} R/R_0$$

$$1 = \frac{1}{2} - \frac{R/R_0}{(1-R/R_0)} - \frac{R/R_0}{\ln(1-R/R_0)(1-R/R_0)}$$

$$\frac{1}{2} \cdot \frac{R_0}{R} \left(1 - \frac{1}{R/R_0} \right) = -1 - \frac{1}{\ln(1-R/R_0)}$$

$$\frac{1}{2} \cdot (R/R_0 - 1) + 1 = \frac{-1}{\ln(1-R/R_0)}$$

$$\frac{1}{2} (R/R_0 + 1) = \frac{1}{\mu \rho x}$$

$$\mu \rho x = \frac{2}{1 + R_0/R}$$

$$= \frac{2}{1 + \frac{1}{1 - e^{-\mu \rho x}}}$$

By the method of iterative guesses

$$\mu \rho x = .6438 \text{ and } R/R_0 = .4747$$

Alternately, a series approximation may be used for the exponential:

$$e^{-a} = 1 - a + \frac{a^2}{2!} - \frac{a^3}{3!} + \dots$$

$$\text{For } a = .64, e^{-a} = .527$$

$$\text{2nd order appx : } e^{-a} \sim .565 \text{ (+7.2\% error)}$$

$$\text{3rd order appx : } e^{-a} \sim .521 \text{ (-1.1\% error)}$$

If the second order approximation is used:

$$\mu\rho x \sim \frac{2}{1 + \frac{1}{1 - 1 + \mu\rho x - \frac{1}{2}(\mu\rho x)^2}}$$

$$\mu\rho x \sim \frac{2 \left(\mu\rho x - \frac{1}{2}(\mu\rho x)^2 \right)}{\mu\rho x - \frac{1}{2}(\mu\rho x)^2 + 1}$$

Rearranging, $(\mu\rho x)^2 - 4(\mu\rho x) + 2 = 0$

$$\mu\rho x \sim .59 \quad \text{and} \quad R/R_0 \sim .46$$

The reader may show that the third order approximation gives a value of

$$\mu\rho x \sim .656 \quad \text{and} \quad R/R_0 \sim .481$$

We again seek the range of thicknesses over which the measurement error is limited to 2x the minimum:

$$\sigma_{\min} = \frac{1}{N^{1/2}} \frac{R/R_0}{\ln(1-R/R_0) (1-R/R_0)} \quad ; \quad R/R_0 = .4747$$

$$\sigma_{\min} = \frac{-1.404}{N^{1/2}}$$

$$\sigma_{\max} = \frac{-2.808}{(Rt)^{1/2}} = \frac{1}{(R't)^{1/2}} \cdot \frac{R'/R_0}{\ln(1 - R'/R_0)(1 - R'/R_0)}$$

$$-4.076 = \frac{(R'/R_0)^{1/2}}{\ln(1 - R'/R_0)(1 - R'/R_0)}$$

By iterative guesses,

$$\mu\rho x' = .06655 \text{ and } R'/R_0 = .06438$$

$$\mu\rho x' = 2.286 \text{ and } R'/R_0 = .8983$$

3.) Fluorescence, forward direction

$$\text{Basic eqn: } R = \frac{KC}{\mu_1 - \mu_2} (e^{-\mu_2 \rho x} - e^{-\mu_1 \rho x})$$

The analysis will be limited to the thin side of the inflection point in the curve. First, let us find where that inflection point is. We find it by locating where the slope is zero:

$$\frac{dR}{d(\rho x)} = \frac{KC}{\mu_2 - \mu_1} \left\{ -\mu_2 e^{-\mu_2 \rho x} + \mu_1 e^{-\mu_1 \rho x} \right\} \equiv 0$$

$$\mu_2 e^{-\mu_2 \rho x} = \mu_1 e^{-\mu_1 \rho x}$$

$$\frac{\mu_2}{\mu_1} = e^{-(\mu_1 - \mu_2) \rho x}$$

$$\ln\left(\frac{\mu_2}{\mu_1}\right) = e^{-(\mu_1 - \mu_2)\rho x}$$

Maximum is at:

$$(\rho x) = -\ln\left(\frac{\mu_2}{\mu_1}\right) \div (\mu_1 - \mu_2)$$

Let's look at some examples:

$$a) \mu_2 \rightarrow \mu_1, \text{ ie, } \mu_2 = \mu_1 + \Delta$$

$$(\rho x) = -\ln(1 + \Delta/\mu_1) \div (-\Delta)$$

$$= 1/\mu_1$$

$$\mu_1 \rho x = 1$$

$$R_{\max} = \frac{KC}{-\Delta} \left(e^{-(\mu_1 + \Delta)\rho x} - e^{-\mu_1 \rho x} \right)$$

$$= + \frac{KC}{\Delta} e^{-\mu_1 \rho x} (1 - e^{-\Delta \rho x})$$

$$= + \frac{KC}{\Delta} e^{-\mu_1 \rho x} (\Delta \rho x) = KC(\rho x) e^{-\mu_1 \rho x} = .368 KC(\rho x)$$

$$R_o = \frac{KC}{\mu_1 + \mu_2} = \frac{KC}{2\mu_1}$$

$$\frac{R_{\max}}{R_o} = .736$$

b) $(\mu_2) = 2\mu$ • This is approximately the case for gold fluorescence excited by Ag $K\alpha$

$$(\rho x) = - \ln(2) \div (-\mu_1) = \frac{.693}{\mu_1}$$

$$\mu_1 \rho x = .693$$

$$R_{\max} = \frac{KC}{-\mu_1} \left(e^{-2\mu_1 \rho x} - e^{-\mu_1 \rho x} \right)$$

$$= \frac{KC}{\mu_1} e^{-\mu_1 \rho x} \left(1 - e^{-\mu_1 \rho x} \right)$$

$$= \frac{KC}{\mu_1} \times .25$$

$$R_o = \frac{KC}{\mu_1 + \mu_2} = \frac{KC}{3\mu_1}$$

$$\frac{R_{\max}}{R_o} = .75$$

$$c) \mu_2 \gg \mu_1$$

Let $\mu_2 = A\mu_1$, where A is a large number

$$\langle \rho x \rangle = \frac{1}{A\mu_1} \ln A$$

$$\mu_1 \rho x = \frac{1}{A} \ln A \quad ; \quad \mu_1 \rho x = .26 \text{ when } A \sim 10$$

$$\begin{aligned} R_{\max} &= \frac{KC}{A\mu_1} \left(e^{-A\mu_1 \rho x} - e^{-\mu_1 \rho x} \right) \\ &= \frac{KC}{A\mu_1} e^{-\mu_1 \rho x} \left(1 - e^{-(A-1)\rho x} \right) \end{aligned}$$

$$R_0 = \frac{KC}{A\mu_1}$$

$$\frac{R_{\max}}{R_0} = e^{-\mu_1 \rho x} \quad \text{when } A \gg 1$$

$$\frac{R_{\max}}{R_0} \sim .79 \text{ when } A \sim 10$$

$$\sim 1 \text{ when } A \rightarrow \infty$$

We see from the foregoing examples that

$$R_{\max} \sim 3/4 R_0$$

where R_{\max} is the highest measurable count rate in the forward direction and R_0 is the highest (i.e., saturation) count rate in the back direction.

The range of values for μ_2 is

$$\mu_1 < \mu_2 \lesssim 10 \mu_1$$

Since we are limiting the analysis to the thin side of the inflection point, the examples show that the range of $(\mu_1 + \mu_2)\rho x$ is zero to about 2 to ~ 2.8

We again seek the minimum error in the measurement of areal density.

The starting eqn is
$$R = \frac{KC}{\mu_1 - \mu_2} \left(e^{-\mu_2 \rho x} - e^{-\mu_1 \rho x} \right)$$

The calibration factor is measured by fluorescence in the backware direction:

$$R_0 = \frac{KC}{\mu_1 + \mu_2}$$

$$K = \frac{R_0(\mu_1 + \mu_2)}{C}$$

so that
$$\frac{R}{R_0} = \frac{(\mu_1 + \mu_2)}{(\mu_1 - \mu_2)} \left(e^{-\mu_2 \rho x} - e^{-\mu_1 \rho x} \right) = \frac{N}{R_0 t}$$

In order to solve for the areal density, a series approximation or an iterative method must be used. With larger values for the exponential term, too many terms in the series approximation are required to be very useful, so an iterative method must be used. However, we already know from the back direction analysis that the optimum thickness is when $\mu\rho x \sim 0.6$. This value for the exponential is more or less adequately represented by a second order approximation (error < 6%).

$$\frac{R}{R_0} = \frac{\mu_1 + \mu_2}{\mu_1 - \mu_2} \left\{ 1 - \mu_2 \rho x + \frac{1}{2} (\mu_2 \rho x)^2 - 1 + \mu_1 \rho x - \frac{1}{2} (\mu_1 \rho x)^2 \cdot \cdot \cdot \right\}$$

$$= \frac{\mu_1 + \mu_2}{\mu_1 - \mu_2} \left\{ (\mu_1 - \mu_2) \rho x - (\mu_1 - \mu_2) (\mu_1 + \mu_2) (\rho x)^2 - \cdot \cdot \cdot \right\}$$

$$= (\mu_1 + \mu_2) \rho x - \frac{1}{2} (\mu_1 + \mu_2) (\rho x)^2 - \cdot \cdot \cdot$$

$$(\rho x)^2 - \frac{2}{\mu_1 + \mu_2} (\rho x) + \frac{2R/R_0}{(\mu_1 + \mu_2)^2} + \cdot \cdot \cdot = 0$$

$$(\rho x) \approx \frac{1}{(\mu_1 + \mu_2)} \left\{ 1 - (1 - 2R/R_0)^{1/2} \right\}$$

This is exactly the same expression as for fluorescence in the backward direction, as may have been anticipated. Therefore, we can use the result from that analyses:

minimum error in (ρx) when $\mu\rho x \sim .64$

By using numerical examples, it is found empirically that:

minimum error in (ρx) is at $\mu_{\rho x} = .52$ and range for doubling the error is $\mu_{\rho x} = .067$ to 1.5 .

Graphs of relative errors follow.

THICKNESS MEASUREMENT BY ABSORPTION

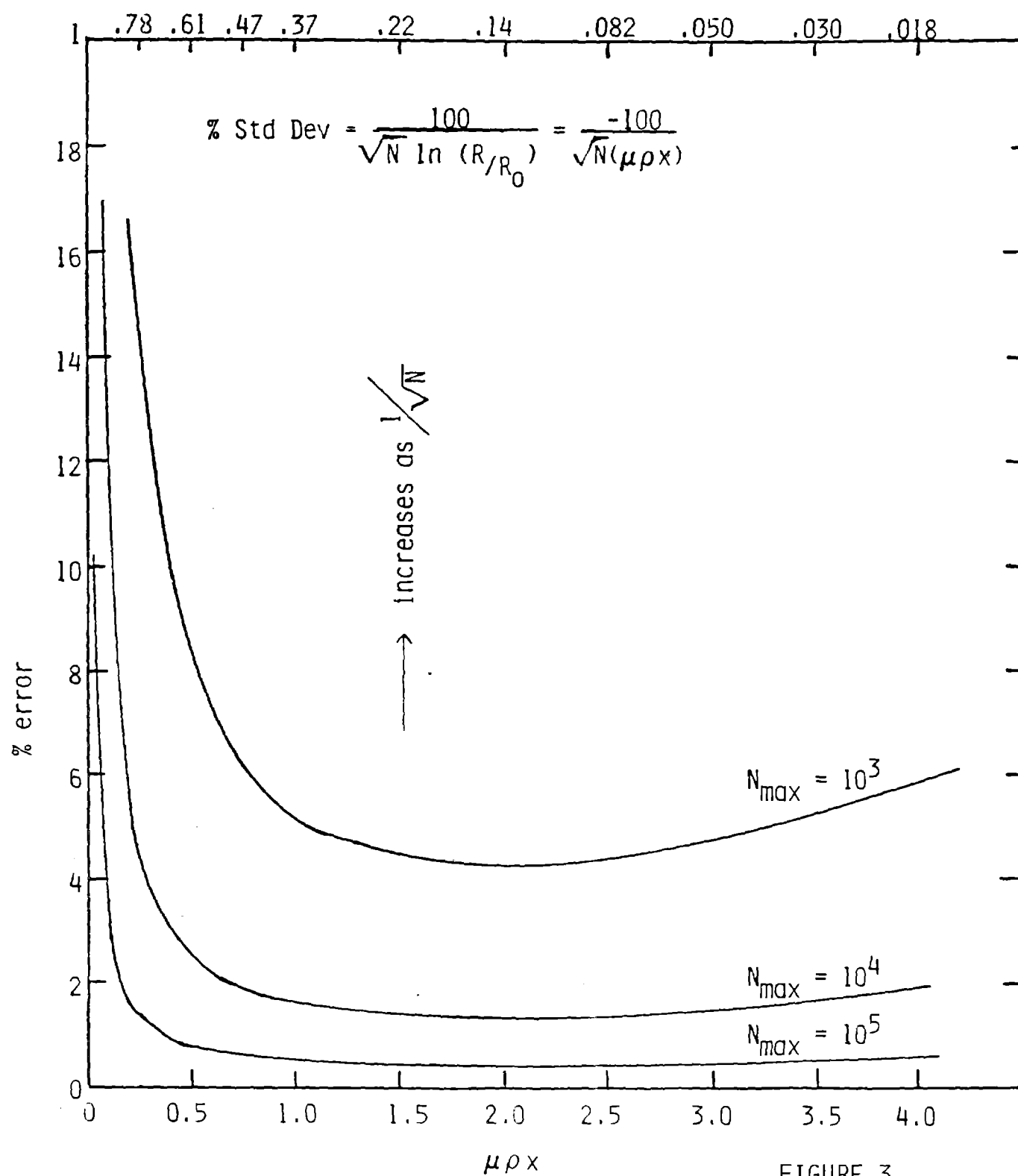


FIGURE 3.

THICKNESS MEASUREMENT BY FLUORESCENCE (Back-direction)

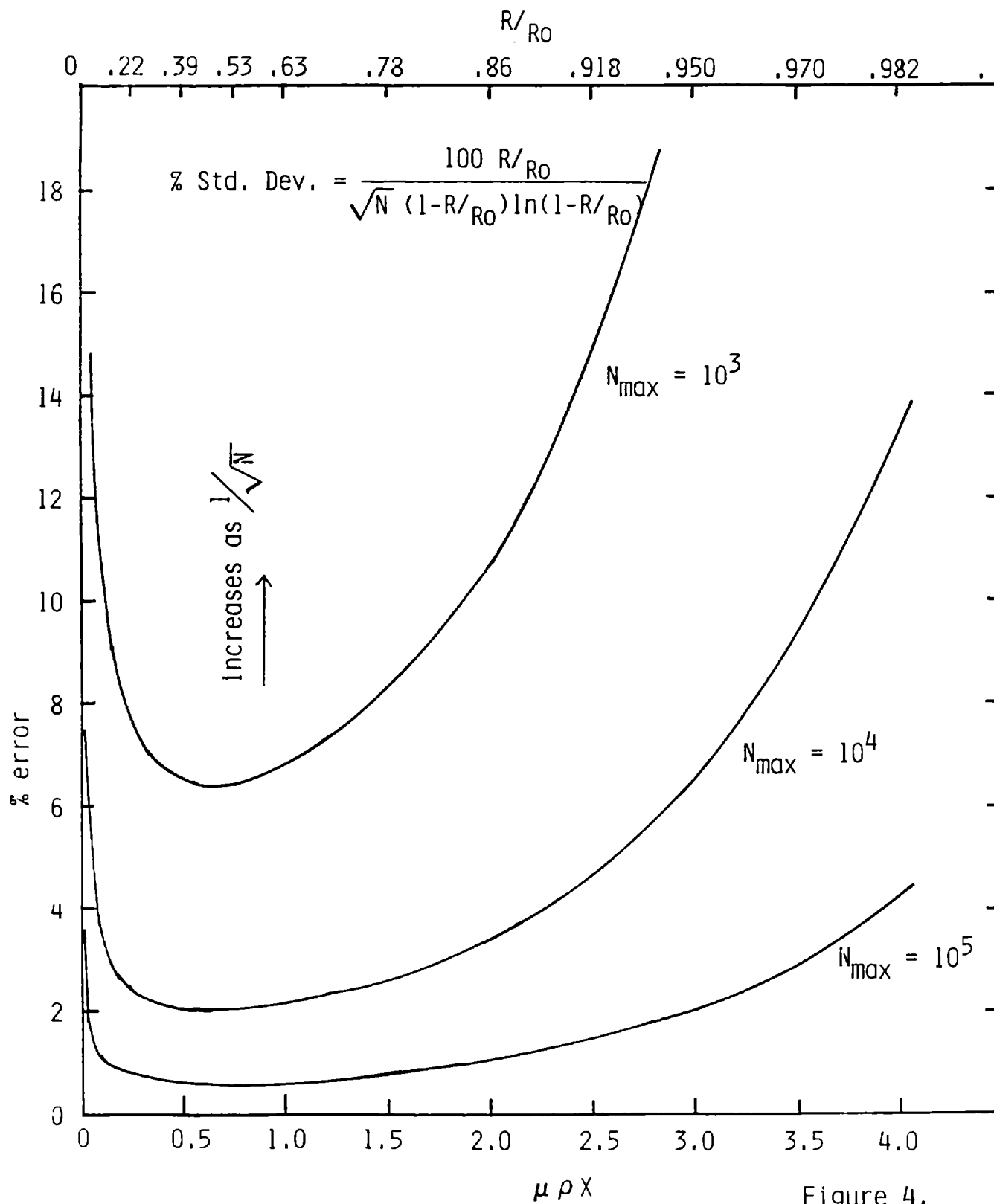


Figure 4.

THICKNESS MEASUREMENT BY FLUORESCENCE THROUGH FILM

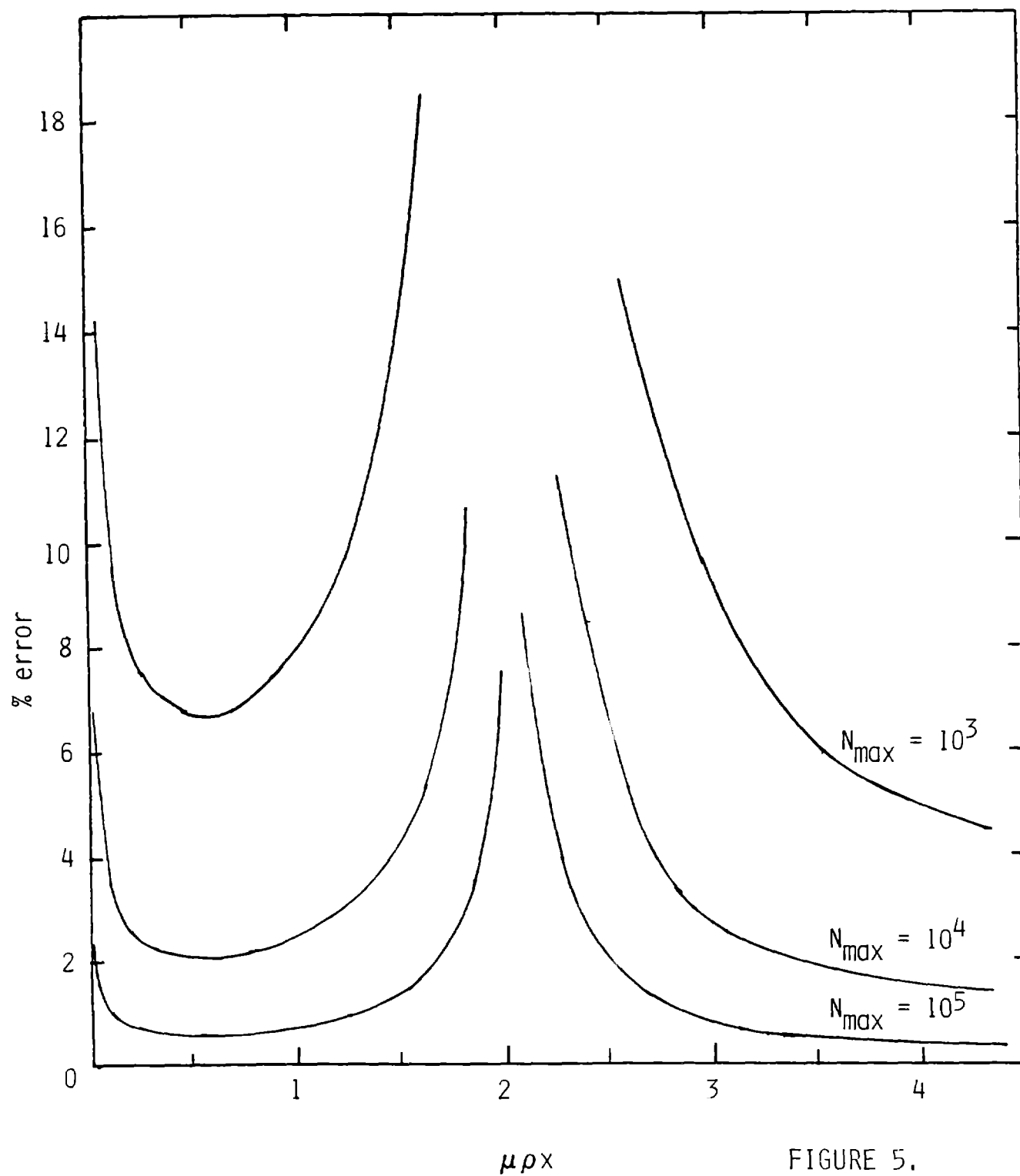


FIGURE 5.